

UNIVERSITY OF BELGRADE  
TECHNICAL FACULTY BOR

**52<sup>nd</sup> International October Conference on  
Mining and Metallurgy**



**PROCEEDINGS**

Edited by

**Saša Stojadinović**

and

**Dejan Petrović**

**November 29<sup>th</sup> – 30<sup>th</sup> 2021**

**Bor, Serbia**

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## TABLE OF CONTENTS

Aleksandra Milosavljević	
<b>THE COMPLEXITY OF SEM-EDS – WHAT AFFECTS THE QUALITY OF OBTAINED RESULTS?</b>	<b>1</b>
Zoran Karastojković, R Perić, M Srečković	
<b>LASER QUENCHING OF CUTTING TOOL STEELS - A REVIEW</b>	<b>5</b>
Slavica Miletić, D Bogdanović, E Požega	
<b>IMPACT OF EXTRAORDINARY SECURITY MEASURES TO EMPLOYEES DURING THE PANDEMIC COVID-9</b>	<b>15</b>
Daniela Grigorova, R Paunova	
<b>KINETIC STUDY OF SOLID-PHASE REDUCTION OF POLYGRADIENT IRON-CONTAINING MATERIAL</b>	<b>19</b>
Emina Požega, D Simonović, S Marjanović, M Jovanović, L Gomidželović, M Mitrović, Z Stanojević Šimšić	
<b>PART I: WHAT MAKES A GOOD THERMOELECTRIC</b>	<b>23</b>
Emina Požega, D Simonović, S Marjanović, M Jovanović, L Gomidželović, M Mitrović, S Miletić	
<b>PART II: WHAT MAKES A GOOD THERMOELECTRIC</b>	<b>27</b>
Dragan Manasijević, Lj Balanović, I Marković, M Gorgievski, U Stamenković, K Božinović, D Minić, M Premović	
<b>STUDY OF MICROSTRUCTURE AND THERMAL CONDUCTIVITY OF THE Ag–Bi–Sn ALLOYS</b>	<b>31</b>
Vladimir S. Topalović, S Matijašević, S Grujić, J Stojanović, J Nikolić, V Savić, S Zildžović	
<b>THE INFLUENCE OF THE PARTICLE SIZE ON CRYSTALLIZATION OF GLASS POWDERS FROM THE SYSTEM <math>\text{Li}_2\text{O}-\text{Al}_2\text{O}_3-\text{GeO}_2-\text{P}_2\text{O}_5</math></b>	<b>35</b>
Vesna Marjanović, R Marković, V Krstić	
<b>TECHNOLOGIES FOR PHYSICAL TREATMENT OF WATER CONTAINING SELENIUM: A REVIEW</b>	<b>39</b>
Vesna Marjanović, R Marković, V Krstić	
<b>TECHNOLOGIES FOR BIOLOGICAL TREATMENT OF WATER CONTAINING SELENIUM: A REVIEW</b>	<b>43</b>
Milenko Jovanović, M Mikić, M Maksimović, D Kržanović, R Rajković, E Požega	
<b>USAGE SPECIFICS OF GEOGRIDS</b>	<b>47</b>

Srećko Manasijević, Z Zovko Brodarac, N Dolić, M Djurdjević, R Radiša	
<b>INTERMETALLIC BONDING BETWEEN A RING CARRIER AND AN ALUMINUM PISTON ALLOY</b>	<b>51</b>
Snežana Šarboh	
<b>PATENTED INVENTIONS OF LJUBOMIR KLERIĆ</b>	<b>55</b>
Miomir Mikic, M Jovanović, R Rajković, D Kržanović, E Požega	
<b>DEGRADED AREA OF VELIKI KRIVELJ QUARRY RECULTIVATION</b>	<b>59</b>
Dragana Adamović, D Ishiyama, H Kawaraya, O Yasumasa	
<b>EFFECTS OF TAILINGS ON GROUNDWATER ALONG BOR AND BELA RIVERS IN THE BOR MINING AREA, EASTERN SERBIA</b>	<b>63</b>
Ana Kostov, Z Stanojević Šimšić, A Milosavljević,	
<b>CHARACTERIZATION OF ALLOYS CuAlAu0.5</b>	<b>67</b>
Marija Milenković, V Jovanović, J Paunković, V Krstić	
<b>MULTICRITERIA ANALYSIS OF THE LEVEL OF SUSTAINABLE DEVELOPMENT OF THE TOPLICA DISTRICT USING THE ELECTRE METHOD</b>	<b>71</b>
Daniel Kržanović, R Rajković, D Stevanović, M Mikić, M Jovanović, S Petrović	
<b>LONG-TERM PLANNING OF MINING THE LEAD AND ZINC ORE DEPOSIT IN THE BRSKOVO ORE FIELD, THE REPUBLIC OF MONTENEGRO</b>	<b>75</b>
Radmilo Rajković, D Kržanović, M Mikić, M Jovanović	
<b>CALCULATION OF SAFETY DISTANCE FOR THE OPERATION OF MINING EQUIPMENT IN THE WORKING ENVIRONMENT WITH WEAKENED CHARACTERISTICS AT THE OPEN PIT "NORTH MINING DISTRICT" OF THE COPPER MINE MAJDANPEK</b>	<b>79</b>
Zdenka Stanojević Šimšić, A Kostov, A Milosavljević, E Požega	
<b>HARDNESS, MICROHARDNESS AND ELECTROCONDUCTIVITY OF ALLOYS WITH VARIABLE Cu CONTENT IN Cu-Al-Ag SYSTEM</b>	<b>83</b>
Miodrag Banješević	
<b>STRATIGRAPHY AND AGE OF ROCK UNITS AND MINERALIZATION IN THE TIMOK MAGMATIC COMPLEX AND THE BOR METALLOGENIC ZONE – A REVIEW</b>	<b>87</b>
Milan Radivojević, Z Stević, M Tanasković	
<b>DUALPHASED FOURWAY INTERSECTION REGULATED BY TRAFFIC LIGHTS WITH FIXED AND ADAPTIVE MOD OF OPERATION</b>	<b>93</b>
Filip Gramić, N Rančić, S Filipović, J Đorđević	
<b>USE OF COPPER TAILING AND COPPER SLAG IN 3D PRINTED CONCRETE PROCESSES</b>	<b>97</b>
Filip Gramić, N Rančić, S Filipović, J Đorđević,	
<b>POSSIBILITY OF USING MINING WASTE IN THE PRODUCTION OF BRICK PRODUCTS</b>	<b>101</b>

Stepan O. Vidysh

**GOLD-SILVER ALLOYS ANODIC DISSOLUTION RESEARCH IN HYDROCHLORIC ACID ELECTROLYTES** 105

Milan Gorgievski, M Marković, D Božić, Vr Stanković, N Štrbac, V Grekulović, M Zdravković

**ADSORPTION ISOTHERMS FOR COPPER IONS ADSORPTION ONTO WALNUT SHELLS** 109

Miljan Marković, M Gorgievski, N Štrbac, V Grekulović, A Mitovski, K Božinović, M Zdravković

**pH AND CONDUCTIVITY CHANGE DURING THE RINSING AND ADSORPTION OF COPPER IONS ONTO WALNUT SHELLS** 113

Vesna Grekulović, A Mitovski, M Rajčić Vujasinović, N Štrbac, M Zdravković, M Gorgievski, M Marković

**ELECTROCHEMICAL BEHAVIOR OF COPPER IN CHLORIDE MEDIUM IN THE PRESENCE OF WALNUT SHELL MACERATE** 117

Marija Šljivić-Ivanović, S Dimović, I Jelić,

**EXPERIMENTAL DESIGN APPROACH IN RADIONUCLIDE SORPTION** 121

Ivana Jelić, A Savić, M Šljivić-Ivanović, S Dimović

**INFLUENCE OF SILICA FUME ON SCC CONCRETE PROPERTIES** 125

Milan Radovanović, A Simonović, M Petrović Mihajlović, Ž Tasić, V Nedelkovski, M Antonijević

**L-LYSINE AS CORROSION INHIBITOR OF STAINLESS STEEL IN RINGER'S SOLUTION** 129

Dragana Marilović, M Trumić, M Trumić, Lj Andrić

**THE INFLUENCE OF CALCIUM IONS ON DEINKING FLOTATION RECOVERY UNDER DIFFERENT CONDITIONS** 133

Dragana Medić, S Milić, S Alagić, M Nujkić, S Đorđević, A Papludis

**OPTIMIZATION OF CATHODIC MATERIAL LEACHING PROCESS IN ACID-SULPHATE SOLUTION** 137

Milijana Mitrović, D Gusković, S Marjanović, B Trumić, E Požega, U Stamenković, J Petrović

**OBTAINING MULTILAYER COPPER STRIPS BY ARB (ACCUMULATIVE ROLL BONDING) ROLLING PROCESS** 141

Nataša Đorđević, S Mihajlović, N Obradović, A Peleš, S Filipović

**THE INFLUENCE OF HIGH COMPACTION PRESSURE ON CORDIERITE-BASED CERAMICS** 145

Nataša Đorđević, S Mihajlović, M Sokić, B Marković

**SEM AND X-RAY ANALYSES OF SINTERED MgO / Bi<sub>2</sub>O<sub>3</sub> BINARY SYSTEM** 149

Ivana Ilić, J Sokolović, M Trumić, Z Stirbanović	
<b>COMPARATIVE RESULTS OF COPPER FLOTATION FROM SLAG BEFORE AND AFTER THE PROCESS OF MAGNETIC CONCENTRATION</b>	<b>153</b>
Daniela Grigorova	
<b>FERROSILICON OBTAINING USING IRON-SILICATE –FAYALITE</b>	<b>157</b>
Slavica Mihajlović, M Jovanović, N Đorđević, A Patarić, M Vlahović, V Kašić	
<b>THE CLAY PRELIMINARY TESTING FROM MUNICIPALITY AREA OF REKOVAC</b>	<b>161</b>
Milan Milosavljević, M Premović, D Minić, Dn Mansijević, Ar Đorđević, M Kolarević	
<b>EXPERIMENTAL AND THERMODYNAMIC STUDY OF ISOTHERMAL SECTIONS AT 600 °C AND 400 °C OF TERNARY Bi-Cu-Ge SYSTEM</b>	<b>165</b>
Aleksandar Đorđević, D Minić, M Premović, D Mansijević, M Milosavljević, V Ristić	
<b>STUDY OF TEMPERATURE PHASE TRANSFORMATION OF THE TERNARY Bi-Cu-Ge SYSTEM</b>	<b>169</b>
Aleksandar Savić, I Jelić, M Šljivić-Ivanović, S Dimović, N Pudar, A Pfandler	
<b>RECYCLED COARSE AGGREGATE AND FLY ASH EFFECT ON COMPRESSIVE STRENGTH OF SELF-COMPACTING CONCRETE</b>	<b>173</b>
Vladan Kašić, D Životić, V Simić, A Radosavljević-Mihajlović, J Stojanović, S Mihajlović, M Vukadinović	
<b>FORECAST RESOURCES OF ZEOLITHIC TUFFS OF SERBIA</b>	<b>177</b>
Vladan Kašić, A Radosavljević-Mihajlović, S Radosavljević, J Stojanović, S Mihajlović, M Vukadinović	
<b>GEOLOGICAL AND MINERAL CHARACTERISTICS OF ZEOLITHIC TUFF TOPONICA DEPOSITS NEAR KOSOVSKA KAMENICA</b>	<b>181</b>
Konstantin Petkov, V Stefanova, P Iliev	
<b>METHOD FOR UTILIZATION OF THE SULFURIC ACID OBTAINED DURING AUTOCLAVE DISSOLUTION OF PYRITE CONCENTRATE</b>	<b>185</b>
Stefan Đorđević, D Ishiyama, Y Ogawa, Z Stevanović, O Osenyeng, D Adamović, V Trifunović	
<b>MONITORING OF pH VALUE AND CONCENTRATION OF COPPER IN RIVERS DOWNSTREAM FROM BOR MINE IN PERIOD 2015-2021</b>	<b>189</b>
Viša Tasić, M Cocić, B Radović, T Apostolovski-Trujić	
<b>CHEMICAL COMPOSITION OF PARTICULATE MATTER IN THE INDOOR AIR AT THE TECHNICAL FACULTY IN BOR (SERBIA)</b>	<b>193</b>
Snežana Ignjatović, I Vasiljević, M Negovanović	
<b>DEFINING STRUCTURAL CORRELATION USING OF TOTAL HORIZONTAL GRADIENT</b>	<b>197</b>

Velizar Stanković, M Janošević

**INCREASING THE CAPACITY OF THE COPPER SMELTING COMPANY IN THE COMPANY  
"SERBIA ZIJIN COPPER" - CHALLENGES AND CONSEQUENCES TO THE ENVIRONMENT** 201

Vladimir Jovanović, D Todorović, B Ivošević, D Radulović, S Milićević, D Nišić

**CHARACTERIZATION OF PELLET SAMPLES OBTAINED BY PELETIZATION OF LIMESTONE  
AND SEAWEED** 205

Vanja Trifunović, L Avramović, R Jonović, S Milić, S Đorđievski, M Jonović

**HYDROMETALLURGICAL TREATMENT OF ELECTRIC ARC FURNACE DUST IN AIM OF ZINC  
SEPARATION** 209

Jovana Bošnjaković, N Knežević, N Čutović, M Bugarčić, A Jovanović, Z Veličković, S  
Manasijević

**EVALUATION OF ADSORPTION PERFORMANCE OF PHOSPHATES REMOVAL USING CELL-  
MG HYBRID ADSORBENT** 213

Dragan Radulović, Lj Andrić, D Božović, V Jovanović, B Ivošević, D Todorović,

**POSSIBILITY OF USING LIMESTONE FROM "PJEŠIVAČKI DO"-DANILOVGRAD DEPOSIT AS  
FILLER IN VARIOUS INDUSTRY BRANCHES** 217

Predrag Stolić, J Ivaz, D Petrović, Zoran Stević

**ADVANTAGES OF MINING ENGINEERING CURRICULUM REALIZATION USING  
SOLUTIONS BASED ON FREE SOFTWARE** 221

Slađana Krstić, E Požega, S Petrović, S Magdalinović, D Urošević, S Miletić, Z Stojanović  
Šimšić

**QUALITY INVESTIGATION OF SAND FOR THE PRODUCTION OF AGGREGATES ON  
VINOGRADI LOCALITY (DELIBLATSKA PEŠČARA)** 225

Saša Marjanović, D Gusković, M Mitrović, E Požega, B Trumić, U Stamenković

**INFLUENCE OF COLD ROLLING AND ANNEALING ON HARDNESS OF BIMETALLIC STRIP  
Cu– Al** 229

## OBTAINING MULTILAYER COPPER STRIPS BY ARB (ACCUMULATIVE ROLL BONDING) ROLLING PROCESS

Milijana Mitrović<sup>1</sup>, Dragoslav Gusković<sup>1</sup>, Saša Marjanović<sup>1</sup>, Biserka Trumić<sup>2</sup>, Emina Požega<sup>2</sup>, Uroš Stamenković<sup>1</sup>, Jasmina Petrović<sup>1</sup>

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### Abstract

*In this paper, the production of multilayer samples, by joining copper strips, by the rolling process at temperatures below the recrystallization temperature is presented. The newly obtained multilayer samples were then subjected to tensile testing and hardness measurement in order to determine their properties. The obtained results show that with increasing degree of reduction, the tensile strength and hardness of the samples increase. Up to the degree of reduction of 66.5%, the tensile strength and hardness of the samples increase slightly, while at a higher degree of reduction of 66.5%, the growth is much more pronounced.*

**Keywords:** Multilayer copper strips, ARB Roll Bonding, hardness, tensile strength.

### 1. INTRODUCTION

The initial idea for this work was based on the knowledge about the application of ARB (Accumulative Roll Bonding) method for rolling sheets and strips (Figure 1) [1]. This method achieves the required metal reduction with minimal stresses, by cutting the rolled sheets, joining and re-rolling, whereby this procedure can be repeated an unlimited number of times [2]. There is a joining of metals by hot and cold rolling. Making the joint by hot rolling is a more efficient and widely used production method of rolled multilayer semi-finished products. The joint is made by hot rolling from pre-prepared strips packed and joined, and then heated to the temperature required for hot rolling. The application of hot rolling has its basic meaning in the setting to obtain products of smaller thickness than the initial large pieces without intermediate annealing and to facilitate joining, and the joint is achieved at a lower degree of deformation. Cold rolling technology, especially strips rolling, has a disadvantage in terms of the use of expensive equipment for both preparation and rolling. The requirements for large reduction in one pass impose the use of specialized rolling machines with large roller diameters, small rolling width and low rolling speed, as well as a preparation line within the rolling machine. In addition, solving the disadvantages of hot and cold rolling is done by combining procedures, in such a way that the joining is done by some other process, such as explosive joining, and by further hot or cold rolling pieces of the final dimensions are produced [3,4].

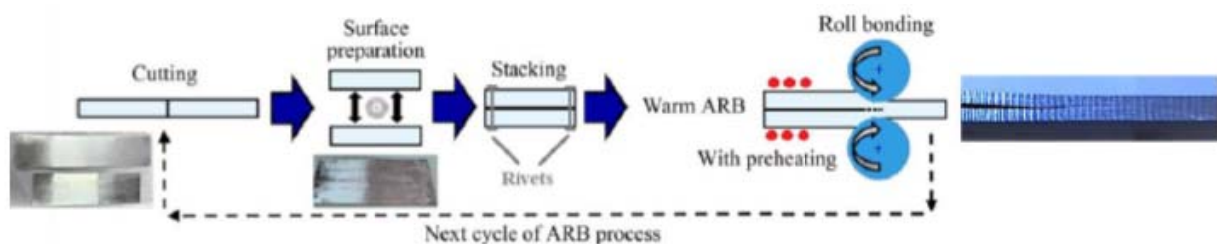


Figure 1. Schematic view of ARB (Accumulative Roll Bonding) rolling process

## 2. EXPERIMENTAL

As a starting material, dip-forming wire in the form of a strip with dimensions 100 x 7 x 1 mm was used, which was rolled on a quarto rolling machine with smooth rollers, diameter  $D = 180$  mm.

Rolling was done by cutting 200 strips 100 mm long, 7 mm wide and 1 mm thick. For degreasing, they were boiled in detergent for about 30 minutes, and then washed with a solution of nitric acid (1: 1 solution), distilled water and finally alcohol. After drying, two strips were joined together, whereby the joining was done by placing copper foil on the ends of the sample. Thus, two-layer samples (2 mm thick) were formed, ready for annealing. The samples were annealed at  $400^\circ\text{C}$  for 10 minutes to reduce the oxidation level of the sample surface. Annealing was performed by inserting the samples into a metal box filled with charcoal. After annealing, rolling was started on a quarto-rolling machine, whereby the obtained samples had a degree of reduction of  $\varepsilon_1 = 40\%$ . Such samples were immediately deposited in a charcoal box, annealed at  $400^\circ\text{C}$  for about 10 minutes and re-rolled, with a reduction degree of  $\varepsilon_2 = 44.1\%$ . The obtained sample consisted of two layers with a total reduction of  $\varepsilon_{\text{uk}} = 66.5\%$ . After that, two two-layer samples were joined, of course, before their joining, the sample was washed and cleaned again, in order to remove impurities. Joining of these samples was done with copper foil at the ends of the sample. The samples were then annealed for 10 minutes at  $400^\circ\text{C}$  and then rolled. The degree of reduction after rolling is  $\varepsilon_3 = 48.5\%$ . The obtained samples had four layers. The obtained samples were washed again for degreasing and cleaning, joined in pairs, annealed and rolled, however the process of joining these samples and obtaining eight layers in the sample was not successful. As a final result, a sample with four layers was obtained. The total degree of reduction in relation to the initial sample is  $\varepsilon_{\text{uk}} = 83\%$ . The flow of the whole experiment is schematically shown in Figure 2.

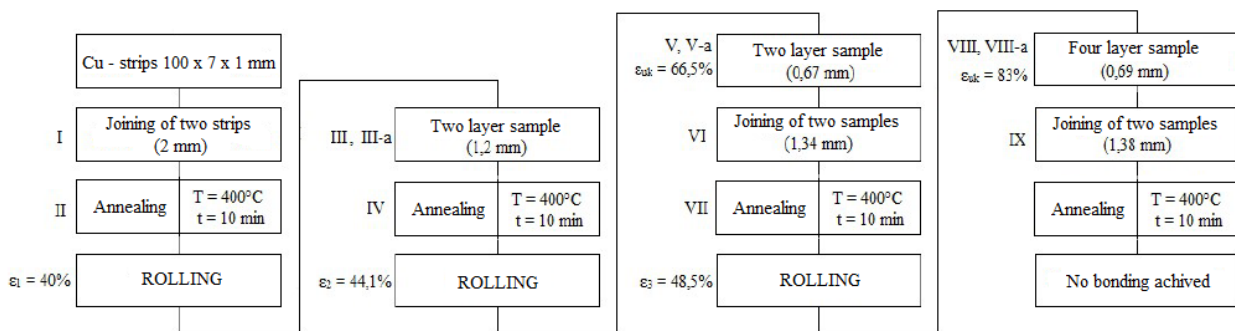


Figure 2. Schematic view of the experiment flow

## 3. RESULTS AND DISCUSSION

Visual inspection of the samples has shown that quality bimetallic strips of small thickness below 0.7 mm can be obtained by rolling.

Flaking was not observed in any of the examined samples. The strips have smooth surfaces, even widths along the length, even thicknesses along the length, and the edges are smooth without cracks.

The results of the change in tensile strength and hardness of the samples depending on the degree of reduction are presented in Table 1 and Figures 3 and 4.



Table 1. Hardness and tensile strength values depending on the degree of reduction

Sample	Degree of reduction $\epsilon$ (%)	Medium hardness value (HV)	Tensile strength $R_m$ (N/mm <sup>2</sup> )
III	40	103	46,221
III - a	40	102	44,345
V	66,5	109	55,336
V - a	66,5	108	47,826
VIII	83	116	116,422
VIII - a	83	110	84,559

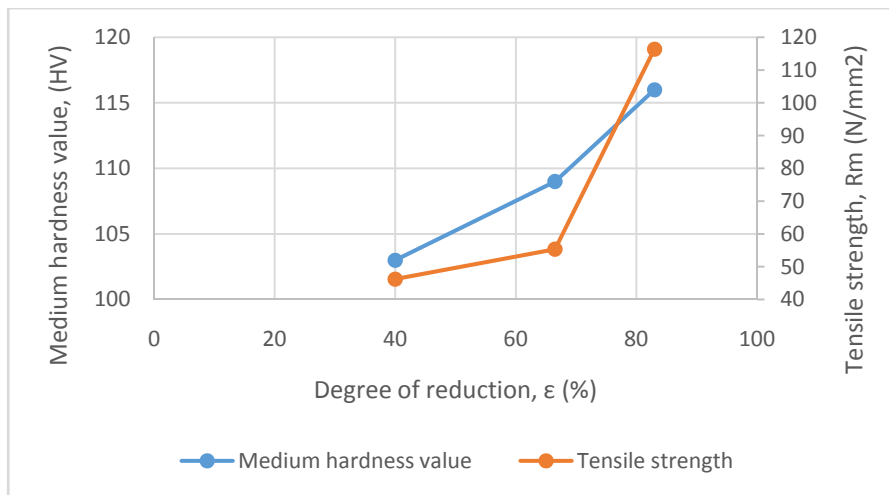


Figure3. Dependence of hardness and tensile strength of samples on the degree of reduction for the I series of samples

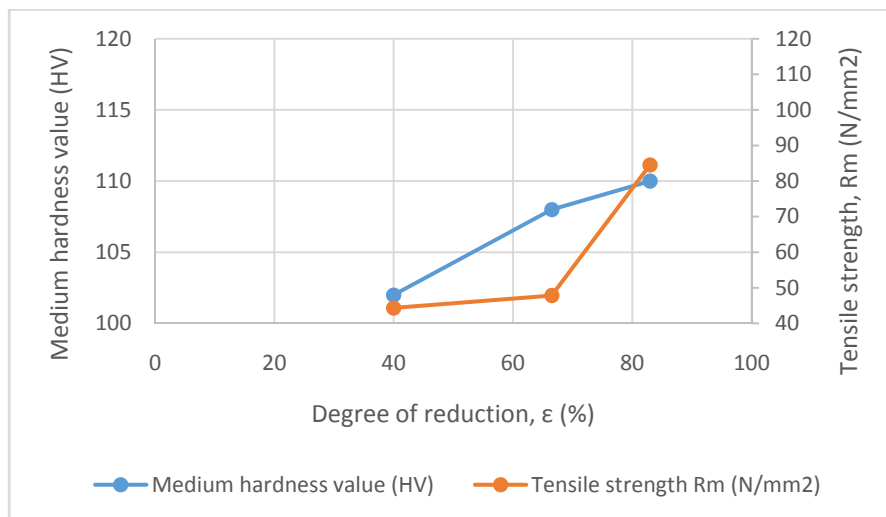


Figure4. Dependence of hardness and tensile strength of samples on the degree of reduction for the II series of samples

The diagrams show that as the total reduction increases, both the hardness and the tensile strength increase.

In the first series of samples, higher values of hardness and tensile strength were observed compared to the second series of samples.

The minimum hardness values, 102 HV and 103 HV, were obtained for samples deformed with a reduction degree of 40%, while the maximum values, 110 HV and 116 HV, were obtained at a

reduction degree of 83%. Tensile strength has values of 44 (N/mm<sup>2</sup>) and 46 (N/mm<sup>2</sup>) to a maximum of 116 (N/mm<sup>2</sup>) and 84.5 (N/mm<sup>2</sup>).

The measured values of hardness and tensile strength for the first series of samples are higher than the measured values of hardness and tensile strength for the second series of samples at given degrees of reduction.

#### 4. CONCLUSION

Based on the obtained results, the following conclusions can be drawn:

- By rolling copper strips, samples less than 0.7 mm thick can be obtained, without flaking, the strips have smooth surfaces, uniform widths along the length, uniform thicknesses along the length, and the edges are smooth and without cracks.
- With increasing degree of reduction, the tensile strength and hardness of the samples increase. Up to the degree of deformation of 66.5%, the tensile strength and hardness of the samples increase slightly, while at a higher degree of reduction than 66.5%, the growth is much more pronounced.
- The measured values of hardness and tensile strength for the first series of samples are higher than the measured values of hardness and tensile strength for the second series of samples at given degrees of reduction.
- Higher values of hardness and tensile strength for samples rolled in the first series compared to the hardness and tensile strength of samples rolled in the second series, are probably due to either slightly shorter heating of samples in the furnace or longer retention of samples in the charcoal box after removal from the furnace and a longer time of transferring samples from the box to the rolling machine.

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